Soft glassy rheology: modelling & measuring strains in amorphous flows

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Outline

- 1 Soft glasses: Phenomenology and SGR model
- 2 Virtual strain analysis
- 3 Shear flow: steady state distributions
- 4 Shear flow: dynamics
- **5** Summary and outlook

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Soft glasses: phenomenology

- Foams, dense emulsions, onion phases, colloidal glasses, clays, pastes, . . .
- Common rheological features:
 - flow curves $\sigma(\dot{\gamma}) \sigma_Y \sim \dot{\gamma}^p \ (0 ,$ $Herschel-Bulkley (if yield stress <math>\sigma_Y \neq 0$) or power-law
 - Nearly 'flat' viscoelastic spectra $G'(\omega)$, $G''(\omega)$ for low frequencies ω (also in cytoskeleton?)
 - Rheological aging
- Suggests common underlying features: arrangements of particles/droplets etc are disordered and metastable
- Analogy with glasses
- Soft glassy rheology approach exploits this; minimal model (based on Bouchaud's trap model)

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SGR Virtual strain Distributions Dynamics Summary

Soft glasses: Linear rheology



FIG. 2. The frequency dependence of the storage G' (solid points) and loss G'' (open points) moduli of a monodisperse emulsion with $r \approx 0.53 \ \mu m$ for $\phi_{eff} = 0.80$ (diamonds), 0.63 (triangles), and 0.60 (circles). The results for the two larger

- Complex modulus for dense emulsions (Mason Bibette Weitz 1995)
- Almost flat $G''(\omega)$: broad relaxation time spectrum, glassy

SGR Virtual strain Distributions Dynamics Summary

Colloidal hard sphere glasses Mason Weitz 1995



Onion phase Panizza et al 1996



- Vesicles formed out of lamellar surfactant phase
- Again nearly flat moduli

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Microgel particles Purnomo van den Ende Vanapalli Mugele 2008



FIG. 1 (color online). G' (open symbols) and G'' (solid symbols) of a 7% w/w suspension at 25 °C plotted versus ω (a) or ωt (b) for $t_w = 3$ (\bigcirc), 30 (\square), 300 (\bigtriangledown), and 3000 s (\triangle). Lines represent the SGR model (x = 0.55, $G_p = 410$ Pa).

- $G''(\omega)$ flat but with upturn at low frequencies
- Aging: Results depend on time elapsed since preparation, typical of glasses

SGR model

- Divide sample conceptually into mesoscopic elements
- Each has local shear strain l, which increments with macroscopic shear γ
- But when strain energy $\frac{1}{2}kl^2$ gets close to yield energy E, element can yield
- Yielding resets l=0, and element acquires new E from some distribution $\rho(E)\sim e^{-E}$
- Yielding is activated by an effective temperature *x*; models interactions between elements (also: thermodynamic interpretation)



SGR model



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Equation of motion

• In dimensionless units (for time, energy)

$$\dot{P}(E,l,t) = -\dot{\gamma}\frac{\partial P}{\partial l} - e^{-(E-kl^2/2)/x}P + \Gamma(t)\rho(E)\delta(l)$$

$$\Gamma(t) = \langle e^{-(E-kl^2/2)/x} \rangle =$$
 average yielding rate

- Macroscopic stress $\sigma(t) = k \langle l \rangle$
- Without shear, P(E,t) approaches equilibrium $P_{\rm eq}(E)\propto \exp(E/x)\rho(E)$ for long t
- Get glass transition if $\rho(E)$ has exponential tail; happens at x=1 if $\rho(E)=e^{-E}$

(possible justification from extreme value statistics)

• For x < 1, system is in glass phase; never equilibrates \Rightarrow aging

SGR predictions

- Flow curves: Find both Herschel-Bulkley (x < 1) and power-law (1 < x < 2)
- Viscoelastic spectra G', $G'' \sim \omega^{x-1}$ are flat near x = 1
- In glass phase (x < 1) find rheological aging, loss modulus $G'' \sim (\omega t)^{x-1}$ decreases with age t
- Steady shear always 'interrupts' aging, restores stationary state
- Stress overshoots in shear startup, nonlinear G' and G'', linear and nonlinear creep, normal stresses (in tensorial version)...

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A broader issue: Defining local strains

- Model assigns local strain for any single configuration
- Harder than coarse graining change of strain between two successive configurations
- Problem: no reference configuration, as in a crystal

Aim

Develop method for assigning local strains and yield energies to material elements, from single snapshots of simulation data

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Defining elements

- Focus on d = 2 (d = 3 can be done but more complicated)
- Make elements circular to minimize boundary effects
- Position circle centres on square lattice to cover all of the sample (with some overlap)
- Once defined, element is co-moving with strain: always contains same particles ("material element")
- Avoids sudden change of element properties when particles leave/enter, but makes sense only up to moderate $\Delta\gamma$
- Measuring average stress in an element is easy but how do we assign strain *l*, yield energy etc for a *given* snapshot?

Virtual strain analysis

- Cannot "cut" an element out of sample and then strain until yield unrealistic boundary condition
- Idea: Use rest of sample as a frame
- \bullet Deform the frame affinely to impose a virtual strain $\tilde{\gamma}$
- Particles inside element relax non-affinely to minimize energy
- Gives energy landscape $\epsilon(\tilde{\gamma})$ of element
- Yield points are determined (for $\tilde{\gamma} > 0$ and < 0) by checking for reversibility for each small $\Delta \tilde{\gamma}$ (adaptive steps)
- Local analysis effectively at T=0 to avoid stochastic effects; for consistency, do steepest descent to nearest global energy minimum of entire configuration first

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Element energy landscape



Extract: minimum energy ϵ_{\min} , strain away from local minimum $l = -\tilde{\gamma}_{\min}$, yield strains γ_{\pm} , yield barriers E_{\pm}

So what is the reference configuration?

- Locally determined
- Stress-free point on virtual energy landscape
- Local strain = virtual strain difference between original configuration and reference
- Doesn't presuppose specific structure for reference configuration (cf. Graner et al's texture tensor)

Local modulus

Quadratic fit of energy near minimum, or linear fit of stress, gives local modulus \boldsymbol{k}



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Systems studied

- Polydisperse Lennard-Jones mixtures (Tanguy et al), quenched to low temperatures ($T=10^{-4}\ll T_{\rm g})$
- Low shear rates $\dot{\gamma}=10^{-4};\,N=10^4$ particles at $\rho=0.925$
- Steady shear driven from the walls (created by "freezing" particles in top/bottom 5% some time after quench)
- Check for stationarity & affine shape of velocity profile before taking data
- Each element contains ≈ 40 particles (diameter ≈ 7)
- Large enough to have near-parabolic energy landscape, small enough to avoid multiple local yield events inside one element (Tanguy, Tsamados et al)

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Simulation lengthscales



Peter Sollich Modelling and measuring local strains

Yield energy distribution



Roughly exponential tail as SGR model would postulate Symmetric: E_{-}/A has same distribution within error bars

Yield strain distributions



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Modulus distribution



Clear spread; not constant as assumed in model

Yield energies remain controlled by yield strains



Dominant effect on variation of E_+ is from yield strain $\gamma_+\text{,}$ not from modulus k

Local strain distribution



Negative l, would need to extend SGR to allow frustration, $l \neq 0$ after yield $(\delta(l) \rightarrow \rho(l|E) \propto (1 - kl^2/2E)^b)$

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Evolution of local strain with time



Some evidence for sawtooth shape assumed by SGR Rearrangement events can perturb many elements at a time

Population picture of *l*-dynamics



Scatter plot of $l_1 = l(\text{after } \Delta \gamma)$ vs $l_0 = l(\text{initial})$ Separation into strain convection and yield events?

SGR Virtual strain Distributions Dynamics Summary

Change in other landscape properties Example of modulus



Stays largely constant between yields as expected; same for yield barriers etc

Strain maps



Significant correlations along principal strain axes $\pm 45^{\rm o}$

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Summary and outlook

- Virtual strain method for assigning local strains, yield energies
- Generic: can be used on configurations produced by any (low-T) simulation
- Also for experimental particle positions, given model of interaction?
- Steady state distributions in shear flow broadly in line with SGR though e.g. local modulus ≠ const
- Dynamics of local strain has typical sawtooth shape; local strain rate is of same order as global one but not identical
- To be done: effect of varying $\dot{\gamma}\text{, }T\text{, }\rho$
- Also: analysis of induced yield events well modelled by effective temperature?

Yield events

- Reversibility check: increment virtual strain, minimize energy, reduce virtual strain again, minimize energy
- \bullet Compare original and final configuration via largest particle displacement Δ
- $\Delta = 0$: reversible, $\Delta > 0$: irreversible
- \bullet Surprisingly, find no obvious lower limit on $\Delta>0$
- $\bullet~$ In practice ignore irreversibility if $\Delta < 0.01$
- $\bullet~{\rm Robust:}~{\rm using}~\Delta<0.1$ gives qualitatively same results